Analysis And Design Of 3- Fluid Heat Exchanger For Utilization Of Waste Heat In The Boiler

Yash shah ,Vani Tarun Kumar ,Parmar Harshil ,Pragnesh Kandoliya

- 1. Student, mechanical V.I.E.R, Gujarat, INDIA
- 2. Student, mechanical V.I.E.R, Gujarat, INDIA
- 3. Student, mechanical V.I.E.R, Gujarat, INDIA
- 4. Asst. Prof., mechanical V.I.E.R, Gujarat, INDIA

ABSTRACT

Our project relates to recover the waste of flue gases heat in boiler and utilize it in pre-heat the boiler feed water and air before they apply to the economizer & air-preheater. The heat which is going to waste from the exhaust is recover by using the piping system connect to exhaust and from there it is connect to Boiler feed water storage where it increase the temperature Of water, then supply to economizer, so it works effectively. And after way another pipe is connected from exhaust air supply, where it increase temp of air, than this air is supply to combustion chamber and combustion faces place very easily. The project Aims at making 3- fluid heat exchanger. It has following features.

1. Efficiency

The efficiency of boiler is increase up to 20% by recover the Waste heat and utilize it in pre –heat feed water and Air.

2. Waste heat utilization

The heat which is going waste from exhaust is utilize by piping system connected form exhaust to feed water storage and air-supply

Keyword: - flue gas waste heat, economizer, air-preheater, combining, 3- fluid heat exchanger

1. INTRODUCTION

1.1 Problem statement

AS per the data we came to know through industry, the main problem associated with is the new concept of 3 fluid heat exchangers is not working. Atmospheric air temperature is about 20C to 25C and water temperature is same as

air. Inlet necessary temperature of air and water is require 75C But, because of wrong pitch length & surface area, require temp is not get. we replace the existing design and made new design in PV elite software.:

1. Improper Design

Because of improper design the waste heat is not going from exhaust to economizer & air-preheater.

2. The heat is not recover.

The amount of heat recovery is very less and other heat is going waste.

1.2 Aim and Objectives of the project

Out aim is to improve the current design of existing model ,which comprise of the all above list problems and eliminate the same by given solution our main aim is to this new design of model to Gujrat metal Industry. We personally believe that this equipment is going to benefit them to a great extent.

1.3 Problem Specification

The problems as specified above are obstructing the application of boiler in industry, otherwise, this new concept Of 3-fluid heat exchanger has a greater scope to work. For the soln of problems we change the piping system of the existing design and made redesign of model. For the maximum amount of heat recovery from join the piping system from exhaust to economizer & air-preheater. As the heat is freely move.

2. DESIGN & MECHANISM

This 3D model had been made in PVLITE 2016 by actual dimension and selected mechanism also.

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Fig -1 : 3D Model

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2.1 MATRERIAL AND DETIAL

Material Properties for SA-516 70

| Material Name : Chemical Composition : | | Temperature (C) | Stress (kgf/cm |
|---|----------------------------|-----------------|----------------|
| Product Form : | | 38 | 1406.1 |
| | rid te | 66 | 1406.1 |
| Class/Thickness : | | 93 | 1406.1 |
| UNS Number : | K02700 | 121 | 1406.1 |
| | | 149 | 1406.1 |
| P Number Thickness : | | 177 | 1406.1 |
| P Number : | | 204 | 1406.1 |
| Group Number : | 2 | 232 | 1406.1 |
| Minimum Tensile Stress : | 4921.5 kof/cm ² | 260 | 1406.1 |
| Minimum Yield Stress : | | 288 | 1385.0 |
| | | 316 | 1364.0 |
| External Pressure Curve : | CS-2 | 343 | 1321.8 |
| Elastic Modulus ID : | 1 | 371 | 1272.6 |
| | - | 399 | 1040.5 |
| Thermal Expansion Coef. ID : | 1 | 427 | 843.7 |
| Material Density : | 7750 kg/m^3 | 454 | 653.9 |
| MDMT Curve 1: | Curve B | 482 | 471.1 |
| MDMT Curve 2 : | Curve D | 510 | 281.2 |
| | | 538 | 175.8 |
| Flange Group : | GR 1.1 | | |
| Listing # : | 1 | | |
| Maximum Temperature : | | | |
| Creep Temperature : | 398 C | | |
| | | L | ОК |
| G10, S1, T2 | F1 (Help) | L | |

3 Why combination of Economizer and Air Pre-Heaters are Provided for Heat Recovery

Boilers are provided with economizer and air pre-heaters to recover heat from the flue gases. An increase of about 20% in boiler efficiency is achieved by providing both economizer and air pre-heaters. Providing economizer alone gives only 8% efficiency increase and so designers provide both.

Most of the high capacity boilers firing coal operate with an efficiency of around 86% on the Higher Heat Value basis. Loss of around 14% can be attributed to various losses of which the dry gas loss is about 35% of the total. When both economizers and air pre-heaters are not provided the boiler efficiency drops to around 66% from 86%.

When air pre-heater is not provided the boiler efficiency will be around 74 % only. Thus we can conserve about 20% extra fuel when we provide both economizers and air pre-heaters in boiler

4 CALCULATION

| INPUT VALUES, Nozzle Descrip Pressure for Reinforcement Calculation | tion: N1 WATER INLET From : 10 ons P 7.031 kgf/cm ² |
|---|---|
| Temperature for Internal Pressure | Temp 93 °C |
| Design External Pressure | Pext 1.05 kgf/cm ² |
| Temperature for External Pressure | Tempex 93 °C |
| Shell Material | SA-516 70 |
| Shell Allowable Stress at Temperatur | re Sv 1406.14 kgf/cm ² |
| Shell Allowable Stress At Ambient | Sva 1406.14 kgf/cm ² |
| Inside Diameter of Elliptical Head | D 2000.00 mm |
| Aspect Ratio of Elliptical Head | Ar 2.00 |
| Head Finished (Minimum) Thickness | s <mark>t 14.0000</mark> mm |
| Head Internal Corrosion Allowance | c 3.0000 mm |
| Head External Corrosion Allowance | co 0.0000 mm |
| Distance from Head Centerline | L1 500.0000 mm |
| User Entered Minimum Design Meta Type of Element Connected to the Material | e Shell : Nozzle SA-106 B |
| Material UNS Number | K03006 |
| Material Specification/Type | Smls. pipe |
| Allowable Stress at Temperature | Sn 1202.25 kgf/cm ² |
| Allowable Stress At Ambient | Sna 1202.25 kgf/cm ² |
| Diameter Basis (for tr calc only) | ID |
| Layout Angle | 90.00 deg |
| Diameter | 6.0000 in. |
| Size and Thickness Basis | Nominal |
| Nominal Thickness | tn 80 |

| Flange Material | SA-105 | | | | |
|---|---------------------------------|--|--|--|--|
| Flange Type We | ld Neck Flange | | | | |
| Corrosion Allowance | can 3.0000 mm | | | | |
| Joint Efficiency of Shell Seam at Noz | zzle E1 1.00 | | | | |
| Joint Efficiency of Nozzle Neck | En 1.00 | | | | |
| Outside Projection h | o 164.6000 mm | | | | |
| Weld leg size between Nozzle and Pa | ad/Shell Wo 10.0000 mm | | | | |
| Groove weld depth between Nozzle a | and Vessel Wgnv 10.0000 mm | | | | |
| Inside Projection h | 0.0000 mm | | | | |
| Weld leg size, Inside Element to She | ll Wi 0.0000 mm | | | | |
| Pad Material | SA-516 70 | | | | |
| Pad Allowable Stress at Temperature | Sp 1406.14 kgf/cm ² | | | | |
| Pad Allowable Stress At Ambient | Spa 1406.14 kgf/cm ² | | | | |
| Diameter of Pad along vessel surface | Dp 340.0000 mm | | | | |
| Thickness of Pad to | e 8.0000 mm | | | | |
| Weld leg size between Pad and Shell | Wp 6.0000 mm | | | | |
| Groove weld depth between Pad and Nozzle Wgpn 8.0000 mm | | | | | |
| Reinforcing Pad Width | 85.8625 mm | | | | |
| ASME Code Weld Type per UW-16 | None | | | | |
| Class of attached Flange | 150 | | | | |
| Grade of attached Flange | GR 1.1 | | | | |

Reinforcement CALCULATION, Description: N1 WATER INLET

| ASME Code, Section VIII, Div. 1, 2015, UG-37 to UG-45 | | | | | |
|---|-----------|--|--|--|--|
| Actual Inside Diameter Used in Calculation | 5.761 in. | | | | |
| Actual Thickness Used in Calculation | 0.432 in. | | | | |

Reqd thk per UG-37(a)of Elliptical Head, Tr [Int. Press]

= (P*K1*D))/(2*Sv*E-0.2*P) per UG-37(a)(3)

=(7.03*0.897*2006.0000)/(2*1406.14*1.00-0.2*7.03)

= 4.5029 mm

Reqd thk per UG-37(a)of Nozzle Wall, Trn [Int. Press]

= (P*R)/(Sn*E-0.6*P) per UG-27 (c)(1)

=(7.03*76.16)/(1202*1.00-0.6*7.03)

= 0.4470 mm

Required Nozzle thickness under External Pressure per UG-28 : 0.5347 mm UG-40, Limits of Reinforcement : [Internal Pressure]

Parall el to Vessel Wall (Diameter Limit) Dl 317.2953 mm

Parallel to Vessel Wall, opening length d 158.6477 mm

Normal to Vessel Wall (Thickness Limit), pad side Tlwp 27.5000 mm

Note : The Pad diameter is greater than the Diameter Limit, the excess will not be considered . Weld Strength Reduction Factor [fr1]:

 $= \min(1, Sn/Sv)$

 $= \min(1, 1202.2/1406.1)$

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= 0.855
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Weld Strength Reduction Factor [fr2]:

```
= \min(1, Sn/Sv)
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= \min(1, 1202.2/1406.1)
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= 0.85

 $= \min(1, Sp/Sv)$

 $= \min(1, 1406.1/1406.1)$

= 1.000

Weld Strength Reduction Factor [fr3]:

= min(fr2, fr4)

 $= \min(0.855, 1.000)$

Weld Strength Reduction Factor [fr4]:

= 0.855

5 ADVANTAGES

1.reducing the fuel costs by means of additional heating energy through efficient heat recovery

- 2. increasing the degree of efficiency up to 11%
- 3. suitable for all waste heat boiler / flue gas boiler / boiler types
- 4. suitable for all standard fuels
- 5. Maximize efficiency and save money
 - 6. Increase steam boiler efficiency and decrease heat loss.
- 7. Save the fuel needed to perform combustion process
- 8. The size of furnace can be smaller because the requirement heat surface is less than witho using economizer.
- 9. Higher feed water temperature tend to reduce boiler thermal stersses, so life boiler increased
- 10. Preheated air increases combustionrate and than increases steam generations rate of biler.

11. due to higher temperature of air, furnace temperature increases ,so low grade coal can be burnt efficiently.

1. CONCLUSIONS

Due to this new design so many conclusion taken which is as follows. By the combination of air pre-heater and economizer in 3 fluid heat exchanger by the efficiency of boiler is increase up to 20% and the losses of flue gases is reduce up to certain level by using it into again in 3 fluid heat exchanger.

6.REFERENCES

1. <u>http://www.brighthubengineering.com/power-plants/34240-economizer-and-air-pre-heaters-are-provided-for-heat-recovery/</u>

2.http://www.maxxtec.com/en/product/automatisch-aus-titel-generieren/heat-exchanger/air-preheater

3<u>http://www1.eere.energy.gov/manufacturing/intensiveprocesses/pdfs/waste_heat_r</u> ecovery.pdf 4. Shower bath economizer test program – james s hall

5.To optimise air preheater design for better perf romance - P.N.SAPKAL, P.R.BAVISKAR, M.J.SABLE, S.B.BARVE.

