MODELING AND SIMULATION OF DISTILLATION COLUMN

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ABSTRACT

Distillation a widely used method for purifying liquids and separating mixtures of liquids into their individual components. It is employed to separate benzene from toluene, methanol or ethanol from water, acetone from acetic acid, and many multicomponent mixtures. This project will comprises the methanol-water mixture distillation. All the parameters that can be varies and affect the distillation process like reflux ratio feed and composition will be studied. Calculation of feed tray and number of stages for the same will be done using McCabe-Thiele Method.

The objective of the project is to study all the parameters that can affect the distillation process. on the modelling and simulation for the process using hysy or using Microsoft Excel.

Keyword: - Distillation, modelling, simulation, Hysys, Methanol water system, excel.

1. Introduction

Distillation is a unit operation that is used in almost every industries for the separation process. Distillation is a widely used method for separating mixtures based on differences in the conditions required to change the phase of components of the mixture. To separate a mixture of liquids, the liquid can be heated to force components, which have different boiling points, into the gas phase. The gas is then condensed back into liquid form and collected. Repeating the process on the collected liquid to improve the purity of the product is called double distillation. Although the term is most commonly applied to liquids, the reverse process can be used to separate gases by liquefying components using changes in temperature and/or pressure. Distillation may result in essentially complete separation (nearly pure components), or it may be a partial separation that increases the concentration of selected components of the mixture. In either case the process exploits differences in the volatility of the mixture's components. In industrial chemistry, distillation is a unit operation of practically universal importance

Modeling is the process of producing a model; a model is a representation of the construction and working of some system of interest.

A simulation of a system is the operation of a model of the system. The model can be reconfigured and experimented with; usually, this is impossible, too expensive or impractical to do in the system it represents. Modeling and simulation is important in research. Representing the real systems either via physical reproductions at smaller scale, or via mathematical models that allow representing the dynamics of the system via simulation, allows exploring system behavior in an articulated way which is often either not possible, or too risky in the real world.

1.1 Model Equations

Q line calculation $q = \frac{\lambda + Cp\Delta t}{\lambda}$ Relative Volatility $\alpha = \frac{\left(\frac{y_{LK}}{\kappa_{LK}}\right)}{\left(\frac{y_{HK}}{\kappa_{HK}}\right)} = \frac{\kappa_{LK}}{\kappa_{HK}}$ A total material balance for tray n $V_{n+1} + L_{n-1} = V_n + L_n$

Material balance around top section use the composition of vapour leaving tray $Y_{n+1}V_{n+1}+X_{n-1}L_{n-1} = Y_nV_n+X_nL_n$

Generalize equation

$$Y_{n+1} = \frac{Rx_n}{L+D} = \frac{1}{R+1}X_D$$

Reboiler Duty Calculation

$$\overline{L} * \Delta H_{vap} + (\overline{L})C_{p,bottom}\Delta T$$

2. Material and Methods

Flowrate	10000 kg/hr = 423.37 Kmol/hr
ΔH of water	40.65
$\Delta \boldsymbol{H}$ of methanol	38.278
C_{p_i} of water	4.18
Column Operating Pressure	Atmospheric Pressure 1 atm
Column condense	Total condenser
Feed Composition	Methanol 40 % Water 60 %
Room Temperature	30 °C
Feed Condition q	1.12
Relative Volatility a	3.10

(Table 2.1 Material and required values)

	F		D		W		
	kmol/hr	%	kmol/hr	%	kmol/hr	%	R
Methanol	169.348	0.4	166.815	0.99	2.5487	0.01	
water	254.022	0.6	1.685	0.01	252.3213	0.99	
total	423.37		168.5		254.87		Cp of water
							Room temperature
		Reboiler	L'*H+L'Cp(tb-				
		duty	tr)				bubble point
			466012.4693	KJ/hr			
			129.4479081	KW			

(Table 2.2 – Reboiler Duty Calculation)

3. Result

0.99	0.98	0.97	0.96	0.95	0.94	0.93	0.92	0.91
No. of trays								
15.06	12.7	11.09	10.1	9.07	8.46	7.73	7.14	6.7
12.84	10.81	9.58	8.68	7.94	7.32	6.8	6.41	5.97
11.79	9.92	8.78	7.98	7.33	6.78	6.36	5.95	5.59
11.03	9.37	8.35	7.59	6.91	6.48	6	5.69	5.32
10.68	8.94	7.98	7.27	6.71	6.23	5.86	5.5	5.11
10.36	8.73	7.8	6.99	6.54	6.02	5.72	5.34	4.96
10.05	8.55	7.63	6.88	6.39	5.92	5.6	5.25	4.89
9.9	8.38	7.48	6.78	6.26	5.84	5.5	5.09	4.83
9.78	8.22	7.35	6.69	6.14	5.78	5.42	5	4.77
9.66	8.07	7.22	6.62	6.04	5.72	5.34	4.96	4.73
	0.99 15.06 12.84 11.79 11.03 10.68 10.36 10.05 9.9 9.78 9.66	0.990.9815.0612.712.8410.8111.799.9211.039.3710.688.9410.368.7310.058.559.98.389.788.229.668.07	0.99 0.98 0.97 15.06 12.7 11.09 12.84 10.81 9.58 11.79 9.92 8.78 11.03 9.37 8.35 10.68 8.94 7.98 10.36 8.73 7.8 10.05 8.55 7.63 9.9 8.38 7.48 9.78 8.22 7.35 9.66 8.07 7.22	0.99 0.98 0.97 0.96 15.06 12.7 11.09 10.1 12.84 10.81 9.58 8.68 11.79 9.92 8.78 7.98 11.03 9.37 8.35 7.59 10.68 8.94 7.98 7.27 10.36 8.73 7.8 6.99 10.05 8.55 7.63 6.88 9.9 8.38 7.48 6.78 9.78 8.22 7.35 6.69 9.66 8.07 7.22 6.62	0.99 0.98 0.97 0.96 0.95 No. of trays 15.06 12.7 11.09 10.1 9.07 12.84 10.81 9.58 8.68 7.94 11.79 9.92 8.78 7.98 7.33 11.03 9.37 8.35 7.59 6.91 10.68 8.94 7.98 7.27 6.71 10.36 8.73 7.8 6.99 6.54 10.05 8.55 7.63 6.88 6.39 9.9 8.38 7.48 6.78 6.26 9.78 8.22 7.35 6.69 6.14 9.66 8.07 7.22 6.62 6.04	0.99 0.98 0.97 0.96 0.95 0.94 No. of trays 15.06 12.7 11.09 10.1 9.07 8.46 12.84 10.81 9.58 8.68 7.94 7.32 11.79 9.92 8.78 7.98 7.33 6.78 11.03 9.37 8.35 7.59 6.91 6.48 10.68 8.94 7.98 7.27 6.71 6.23 10.36 8.73 7.8 6.99 6.54 6.02 10.05 8.55 7.63 6.88 6.39 5.92 9.9 8.38 7.48 6.78 6.26 5.84 9.78 8.22 7.35 6.69 6.14 5.78 9.66 8.07 7.22 6.62 6.04 5.72	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.99 0.98 0.97 0.96 0.95 0.94 0.93 0.92 No. of trays 15.06 12.7 11.09 10.1 9.07 8.46 7.73 7.14 12.84 10.81 9.58 8.68 7.94 7.32 6.8 6.41 11.79 9.92 8.78 7.98 7.33 6.78 6.36 5.95 11.03 9.37 8.35 7.59 6.91 6.48 6 5.69 10.68 8.94 7.98 7.27 6.71 6.23 5.86 5.5 10.36 8.73 7.8 6.99 6.54 6.02 5.72 5.34 10.05 8.55 7.63 6.88 6.39 5.92 5.6 5.25 9.9 8.38 7.48 6.78 6.26 5.84 5.5 5.09 9.78 8.22 7.35 6.69 6.14 5.72 5.34 4.96

(Table 3.1 – Reflux ratio vs Number of Trays)

Xd		.99	0.98	0.97	0.96	0.95	0.94	0.93	0.92	0.91	
R		Reboiler duty									
1.:	5 61	1.39	61.4	60.76	60.12	59.48	58.83	58.23	57.62	57.02	
,	68.	953	69.02	68.28	67.54	66.79	66.03	65.32	64.61	63.9	
2.:	5 76.	517	76.65	75.8	74.95	74.09	73.23	72.42	71.59	70.78	
	8 84.	081	84.28	83.32	82.36	81.4	80.42	79.51	78.58	77.66	
3.:	5 91	l.64	91.9	90.84	89.77	88.7	87.62	86.61	85.57	84.53	
2	4 99.	208	99.53	98.36	97.19	96.011	94.81	93.7	92.56	91.81	
4.:	5 106	5.77	107.15	105.88	104.6	103.31	102.01	100.79	99.54	98.29	
	5 114	1.33	114.78	113.4	112.01	110.62	109.21	107.89	106.53	105.17	
5.:	5 121	1.89	122.4	120.92	119.43	117.92	116.4	114.98	113.52	112.05	
	5 129.	462	130.03	128.44	126.84	125.23	123.6	122.07	120.51	118.93	

(Table 3.2 – Reflux ratio vs Reboiler Duty)





(Graph 3.2 Reflux ratio vs Reboiler Duty)



(Graph 3.4 Reflux ratio vs Reboiler Duty)

4. CONCLUSIONS

We determine the relation between reflux ratio, number of trays and reboiler duty and had concluded that to get high purity reflux ratio should be high which result in high reboiler duty. To minimize the reboiler duty and we had to go for optimum reflux ratio to get desire purity.

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