

# A STUDY ON TECHNOLOGIES USED FOR REMOVAL OF H<sub>2</sub>S & CO<sub>2</sub> FROM NATURAL GAS

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## ABSTRACT

*In this paper we are studying on Technologies used for Removal of H<sub>2</sub>S & CO<sub>2</sub> from Natural Gas. There are mainly two types of acid gas removal processes: adsorption and absorption. Adsorption is a physico-chemical phenomenon in which the gas is concentrated on the surface of a solid to remove impurities. The acid gas removal unit is designed to remove acid sulfur to meet sales gas sulfur and CO<sub>2</sub> specifications. The H<sub>2</sub>S must be removed to meet the sales gas specification of 4 ppmv, or a grain of 100 grams per gas. In addition, COS, mercaptans and other organic sulfur species should be removed.*

**Keyword:** - Gas, CO<sub>2</sub>, H<sub>2</sub>S, COS, Remove, Acid etc.

## 1. INTRODUCTION

At the same time, it is worth exploring potential energy options to deal with the increasing global demand for energy and environmental impacts such as global greenhouse gas (GHG) emissions. As a baseline for most approaches, issues of producing sufficient quantities of energy with high quality, economical feasibility and environmental sustainability are current concerns. One of the important components of the world's energy supply, which meets the above requirement, is natural gas. In addition to its primary importance as a fuel, natural gas is also a source of hydrocarbons for petrochemical feedstocks. Many types of research have been done on the natural gas field because the presence of a high component of methane in natural gas contributes to the production of other potential products such as syrup and high purity hydrogen. Although natural gas is mostly regarded as a "clean" fuel, as compared to other fossil fuels, the natural gas found in reservoir deposits is not necessarily "clean" and free of impurities. Natural gas mainly contains methane as a prevalent element but contains a significant amount of light and heavy hydrocarbons as well as contaminated compounds of CO<sub>2</sub>, N<sub>2</sub>, Hg, He, H<sub>2</sub>S and etc. Thus, impurities must be removed to complete the pipe. -Quality standard specifications as a consumer fuel, increase the calorific value of natural gas, avoid degradation of pipelines and equipment and remove associated process bottlenecks. This paper discusses major advances, process benefits, and limitations of absorption, adsorption, cryogenic, and membrane processes of existing technologies in natural gas refining. In addition, special emphasis is placed on the removal of CO<sub>2</sub> from natural gas as CO<sub>2</sub> is the largest contaminant found in natural gas and a major contributor to global GHG emissions. A comparison between these technologies is also described in terms of advantages and disadvantages. Emerging concepts have been exposed to new approaches in natural gas separation. Finally, future research and development directions of natural gas processing technologies are also presented. The risks posed by CO<sub>2</sub>, H<sub>2</sub>S and other impurities in natural gas (NG) are increasingly dangerous due to their negative consequences in humans, equipment, and the environment. Natural gas can be classified as sweet or sour. It contains methane, ethane, propane, isobutene, n-butane, nitrogen, CO<sub>2</sub>, O<sub>2</sub>, isopentane, n-pentane, hexane, and H<sub>2</sub> [1]. Other gases include helium, hydrogen sulfide, and mercaptans that give the gas its distinctive smell. CO<sub>2</sub> and H<sub>2</sub>S are major pollutants in NG. For easy / safe transport, <50 ppm CO<sub>2</sub> is desired [2]. CO<sub>2</sub> and H<sub>2</sub>S can be trapped using amine solvents, absorption devices, and membranes [3]. Other contaminants, such as carbonyl sulfide, mercaptan, ethane, pentane, etc., are usually removed through distillation and absorption. Gas purification depends on the target – solute solubility, partial vapor pressure of the components and the heat spent during solvent recovery [4], [5]. Absorption of CO<sub>2</sub> from flue gas using several alcohol – amine solvents has been reported [6]. According to Fang and Zhu [7],

the use of amines, carbonates, aqueous ammonia, polymer membranes, ionic liquids and enzymes in the conduction of gas treatment has been recent.

## 2. COMPARISON OF NATURAL GAS PURIFICATION TECHNOLOGIES FOR ACID GAS REMOVAL

Absorption by physical solvents is mostly not recommended at low partial pressures because compression of the gas is relatively not economical for physical absorption. In general, the economics of CO<sub>2</sub> separation are greatly influenced by the partial pressure of CO<sub>2</sub> in feed natural gas. However, if gas is available at high pressures, physical solvents may be a better alternative than chemical solvents. While physical solvents can often be stripped of impurities by reducing pressure without the application of heat, the uptake of chemical solvents is achieved by the application of heat. When the concentrations of acidic gases or other impurities are very high, physical solvents favor chemical solvents. Unlike chemical solvents, physical solvents are non-corrosive, requiring only carbon steel manufacturing. The concentration of heavy hydrocarbons in the feed gas also affects gas treatment options. If the concentration of heavy hydrocarbons is high, a physical solvent may not be the best option due to the high co-absorption of hydrocarbons, especially pentane plus. Unlike synthesis gases, where hydrocarbons do not contain appreciable amounts, natural gas can be a problem for physical solvents as a result of hydrocarbon co-absorption. This is particularly applicable to physical solvents for synthesis gas treatment (Burr and Liddon 2008). Although the adsorption technique is limited to small gas streams and medium pressures due to the complexity of the design, the PSA technique is mostly used in shut-in natural gas wells that typically contain very high N<sub>2</sub>. As a typical example, titanosilicate adsorption (Engelhard Corporation) is used in a vacuum swing adsorption combined with a PSA process to remove N<sub>2</sub> and / or CO<sub>2</sub> from natural gas feed streams (Ritter and Eibner 2007). When natural gas wells contain high CO<sub>2</sub> and H<sub>2</sub>S, the membrane process is best used at high pressures. CO<sub>2</sub> dissociation is accomplished by pressure-driven mass transfer through a permeable membrane, where separation occurs due to differences in the transit rate of different antennas. Although acid gas is usually recovered at low pressures, high purity products containing approximately 95% CO<sub>2</sub> can be obtained with one or two steps, depending on the pressure and percentage recovery of the feed gas. Economic considerations may direct additional pressure and incremental energy requirements to use two-phase separation with increasing feed pressure and / or recombination of gas from the first stage. The cryogenic process, as compared to other methods of separating CO<sub>2</sub>, has the advantage that CO<sub>2</sub> can be obtained at relatively high pressures. However, this advantage can be offset by the need for larger refrigeration.

## 3. SELECTIVE REMOVAL OF H<sub>2</sub>S FROM WATER USING NON-CONDENSED GAS

Carbon dioxide, NCG injection, carbon capture, geothermal. In this study, reinforcement of NCGs (non-condensed gases) released from geothermal plants was investigated. These goals will be achieved with water by injecting CO<sub>2</sub> into the geological reservoir. Both H<sub>2</sub>S and CO<sub>2</sub>, often referred to as "acid gases", are only solubilized in water at atmospheric pressure. Even at elevated pressures, the solubility of these gases in water is not very high; Thus, it is unusual to use water to absorb these gases in commercial-scale gas treatment systems. Alkanolamines and some physical solvents are commonly used for the absorption of acid gases. The stream of vapor from the flash or reboiler, which will be rich in CO<sub>2</sub>, will be returned to the bottom of the absorption column. This process regime allows a substantial improvement in the water's ability to absorb H<sub>2</sub>S from feed NCG, at least (but not eliminate CO<sub>2</sub> absorption). This concept is described in more detail in the rest of this section, and provides the results of the process simulations that were used to characterize it. Water filled with CO<sub>2</sub> and H<sub>2</sub>S from the bottom of the absorption column is subjected to either a low pressure flash or an elevated temperature partial evaporator (reboiler) to remove a large fraction of the CO<sub>2</sub> absorbed by the water. Can go in the absorption column. (Source: Mamrosh, McIntush, Douglas, Fisher, Júlíusson, Gunnarsson, Markússon, Matthíasdóttir, & Arnarson)

**Table 1.1** Case Study for Selective Absorption of H<sub>2</sub>S Using an Absorber Column with Bottoms Flash 35 theoretical stages, 5 bar operating pressure Water feed at 40 kg/s and 30°C (Darryl L. Mamrosh P.E. etal.)

Stream Description	Feed Gas (NCG)	Treated Gas from Absorption Column			
		No Flash	Case 1	Case 2	Case 3
No. Flash Stages		0	2	3	4
Last Stage Pressure, bar		NA	3	2	0.8
Compressor Power, kW		0	21	50	84
Total kg/s	0.500	0.145	0.230	0.288	0.344
H <sub>2</sub> S mole %	25.9	0.031	0.13	1.4	14
CO <sub>2</sub> mole %	51.3	46.2	60	65	58
H <sub>2</sub> S removal %		99.99	99.8	97.4	54.4
CO <sub>2</sub> removal %		57	25	2.8	0.006

Source: Mamrosh, McIntush, Douglas, Fisher, Júlíusson, Gunnarsson, Markússon, Matthíasdóttir, & Arnarson

#### 4. CHARACTERISTICS OF NON-CONDENSED GAS FOR EACH GEOTHERMAL FACILITY

There are many technologies available for the removal of H<sub>2</sub>S from NCG. The six geothermal power plants - Tattapani in Chhattisgarh., Puga in Jammu & Kashmir, Cambay Graben in Gujarat, Manikaran in Himachal Pradesh, Surajkund in Jharkhand, Chhumathang in Jammu & Kashmir - have been operated and / or planned in Iceland by member companies of the Solfix team. These facilities do not currently have H<sub>2</sub>S abatement systems. The summary of NCG characteristics in these features is given in Table 1.2.

**Table 1.1:** Characteristics of NCG for Each Geothermal Facility

Characteristic	Units	Tattapani	Puga	Cambay Graben	Manikaran	Surajkund	Chhumathang
Gas Flow Rate	kg/s	1.582	1.314	0.63	1.5	0.28	1.20
H <sub>2</sub> S Content	mass%	27.06	33.46	4.62	2.62	48.00	6.90
CO <sub>2</sub> Content	mass%	45.70	63.58	94.82	98.88	48.78	73.19
H <sub>2</sub> Content	mass%	1.14	0.49	0.05	0.06	4.66	0.42
N <sub>2</sub> Content	mass%	25.09	2.01	0.68	0.58	0	16.16
O <sub>2</sub> Content	mass%	6.18	0.48	0	0	0	6.27
CH <sub>4</sub> Content	mass%	0.08	0.126	0.02	0.02	0.31	0.05
Ar Content	mass%	0	0	0	0.04	0.19	0.26
H <sub>2</sub> S Flow Rate	ton/day	32.11	34.02	1.66	1.44	7.18	6.57

Source: Mamrosh, McIntush, Douglas, Fisher, Júlíusson, Gunnarsson, Markússon, Matthíasdóttir, & Arnarson

## 5. MEMBRANE TECHNOLOGY

Membrane technologies compete with traditional technologies, such as pressure swing adsorption, temperature swing adsorption, or amine scrubbing in terms of commercial issues [2, 3]. In addition, the uptake of biogas through a membrane usually involves a polymer membrane. A previous study used a thin membrane from a thin hydrophilic composite (TFC) as a different method. Separation of H<sub>2</sub>S by TFC offers future economical possibilities compared to the traditional method [40]. The traditional method decreases in efficiency because of other additional splash steps required to remove water vapor from the biogas stream; However, this step was not required when TFC is used [1]. As a core of separation through the membrane, some components of the raw gases are transported through a thin membrane, while others are retained. Under the membranes studied, several types of membranes have been used as was done in the improvement of the technology. Based on the H<sub>2</sub>S removal results, several parameters need to be investigated. These parameters are the pressure, temperature, permittivity concentration and solubility of gases in the selective water swelling polyamide layer [4]. Methane is an issue in upgrading end product efficiency. The increase of feed pressure and concentration was exaggerated in retaliation. This result was interpreted in a set of data by Dolges et al. (2014) which showed that methane is in concentration increases to 68% per second at 500 kPa, and the lowest number The loss of methane in the permit stream is only 3 vol%. The high Pressure RO membrane is better than low pressure RO membrane. In addition, more H<sub>2</sub>S is removed at lower pressures. The loss of methane in permeate must be considered (References Nurul Noramelya Zulkeflia et al. 2016).

**Table 1.3:** H<sub>2</sub>S efficiency through membrane technique References Nurul Noramelya Zulkeflia et al. (2016)

<i>Technique</i>	<i>Efficiency</i>	<i>References</i>
• High pressure RO (500 kpa)	57 vol.%	Dolejs et al. (2014)
• Low pressure RO (400 kpa)	43 vol.%	
• Micro-porous hydrophobic gas-liquid absorption membrane -High pressure -Low temperature (25 °C)	98%	Wellinger et al. (2005)
• Hollow fibers membrane gas adsorber (HFMDGA) -Pressure: 10 atm	100%	Mahdavian et al. (2012)

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