NUMERICAL ANALYSIS OF SOLAR AIR HEATER DUCT USING STAGGERED INCLINED RIBS WITH A GAP IN STAGGERED ARRANGEMENT

Piyush keshri (MTech Scholar) Scope College of Engineering, Bhopal

Dr.S.K.Nagpure (Asso.Prof.) Scope College of Engineering, Bhopal

ABSTRACT

In this thesis, results of CFD analysis on heat transfer and friction in rectangular ducts with roughened with inclined ribs with a gap in staggered arranged at an inclination with respect to the flow direction. The range of parameters for this study has been decided on the basis of practical considerations of the system and operating conditions of solar air heaters. The numerical investigation encompassed the Reynolds number(Re) range from 2000 to 16,000, relative width to height ratio (W/H) of 8.0, relative gap position is varied to (dt/W & dl/W) of 0.3 & 0.1 to 0.3 & 0.4, relative gap width (g/e) is 1.0, relative roughness height (e/Dh) of 0.045, relative roughness pitch (P/e) of 8, angle of attack (a) of 40^o. The effects of relative gap width on Nusselt number, friction factor and thermo-hydraulic performance Rib roughness on the underside of the top wall of a duct has been found to substantially enhance the heat transfer coefficient. Surface roughness disturbs the laminar sub-layer in the turbulent flow and promotes local wall turbulence that, in turn, increases the heat transfer from the surfaces. The augmentation in heat transfer accompanies a higher pressure drop penalty of the fluid flow. In this work the maximum value is found to be relative gap position is 0.3 & 0.3 at a Reynolds number of 16000.

Keyword: *Reynolds number, Heat transfer, Pressure drop, Friction factor*

Introduction: The SAHs in light of its direct arrangement and low activity and support cost is comprehensively used as a solar collector. The thermal performance of SAHs is an immediate result of its poor heat transfer boundary between the absorber plate and the working fluid, for example, air. The use of artificial roughness on the absorber surface is an effective technique for improving heat transfer between the absorber plate and the working fluid. The roughness element breaks the thermal boundary layer thereby increasing the heat transfer. However, this also increases friction loss resulting in increased pumping power requirements from blower or fan. To reduce friction loss and pumping power, turbulence must be created in the vicinity of the absorber surface so that the sub-layer of the lamina is broken. Many researchers have been carried out on heat transfer enhancement achieved by different ribs. The use of artificial roughness in solar air heaters owes its origin to several investigations carried out in connection with the enhancement of heat transfer in nuclear reactors and turbine blades. Several investigations have been carried out to study effect of artificial roughness on heat transfer and friction factor for two opposite roughened surface by Han[2,3].Han et al.[4-5],Wrieght et al.[7],Lue et al,[8-10],Taslim et al. and Hwang[12],Han and Park[14],Park et al.[15] developed by different investigators . The orthogonal ribs i.e. ribs arranged normal to the flow were first used in solar air heater and resulted in better heat transfer in comparison to that in conventional solar air heater by Prasad k, Mullick S.C. et al [16].Many investigators Gao x sunden B[17],Han J.C,GlicksmanLR,Rohsenow WM[18],Prasad BN,Saini JS[19], TaslimME,LiT,KercherDM[20] ,Webb RL,EckertErg,Goldstein RJ[21] have reported in detail the Nu and f for orthogonal and inclined rib-roughened ducts. The concept of V-shaped ribs evolved from the fact that the inclined ribs produce longitudinal vortex and hence higher heat transfer .In principal ,high heat transfer coefficient region can be increased two folds with V-shape ribs and hence result in even higher heat transfer et al. [20].The beneficial effect on Nu and f caused by V-shaping of ribs in comparison to angled ribs has been experimentally endorsed by several investigators Geo X,Sunden

B{22],Karwa R.[23],KukrejaRT,LueSC,McMillin RD[24],Lau SC,McMillinRD,Han JC[25], for different roughness parameters and duct aspect ratios . In addition ,multiple V-ribs have also been investigated with the anticipation that the more number of secondary flow cells may result in still higher heat transfer et at LanjewarA,BhagoriaJL,Sarviya RM[26],Hans VS,SainiRP,Saini JS[27].Chao et al.[28]examined the effect of an of angle of attack and number of discrete ribs, and reported that the gap region between the discrete ribs accelerates the flow, which increases the local heat-transfer coefficient. In a recent study ,Chao et al.[29] investigated the effect of a gap in the inclined ribs on heat transfer in a square duct and reported that a gap in the inclined rib accelerates the flow and enhances the local turbulence, which will result in an increase in the heat transfer. They reported that the inclined rib arrangement with a downstream gap position shows higher enhancement in heat transfer compared to that of the continuous inclined rib arrangement. Computational studies have also beenused extensively in studying the flow and heat transfereffects in ribbed ducts. The advantage of being able to studyboth the flow and heat transfer in the entire flow field isworth the effort required to simulate ribbed duct flows, butthe whether the channel roughened with ribs of differentshape can improve the heat transfer rate. There have beenattempts undertaken to overcome the adverse effect byvarying the geometry of ribs. Lockett and Hwangemployed the non-invasive optical method of holographicinterferometry to investigate the heat transfer in turbulentflow over square and rounded rib-roughness elements. Theyfound that the heat transfer distribution depends on theReynolds number for the rounded rib, but independent forsquare rib geometry. In both cases, the minimum heattransfer occurred at the base of the rear facing rib wall.

II. Computational Fluid Dynamics

Computational fluid dynamics or CFD is the analysis of systems involving fluid flow, heat transfer and associated phenomena such as chemical reactions by means of computer-based simulation. The technique is very powerful and spans a wide range of industrial and non-industrial application areas. The 2-dimensional solution domain used for CFD analysis has been generated in ANSYS version 14.5 (workbench mode) as shown in Fig.1.The solution domain is a horizontal duct with broken arc shaped ribs combined with staggered rib roughness on the absorber plate at the underside of the top of the duct while other sides are considered as smooth surfaces.

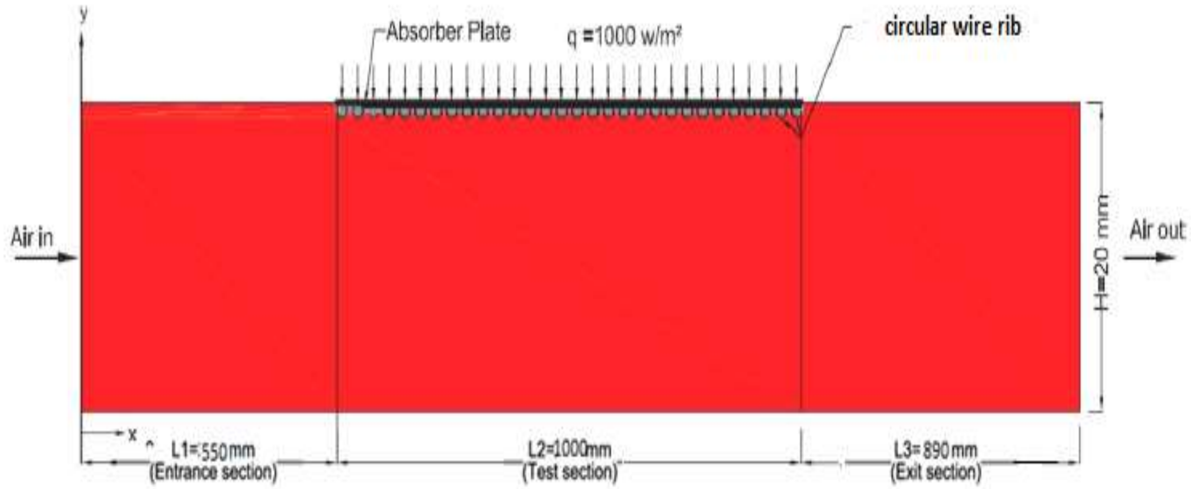
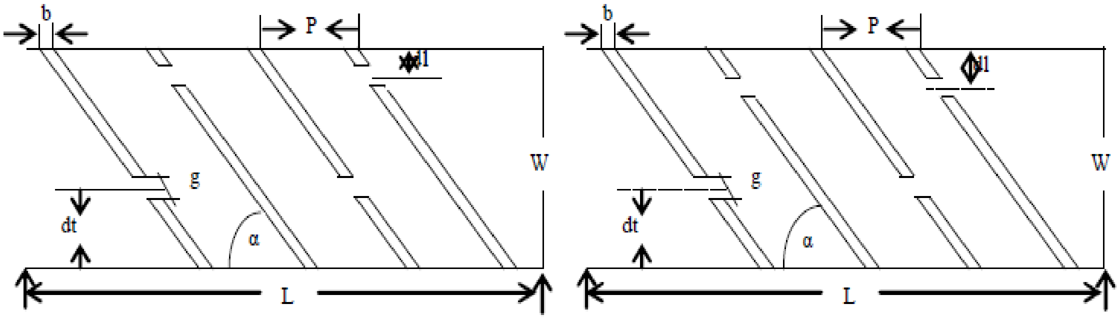
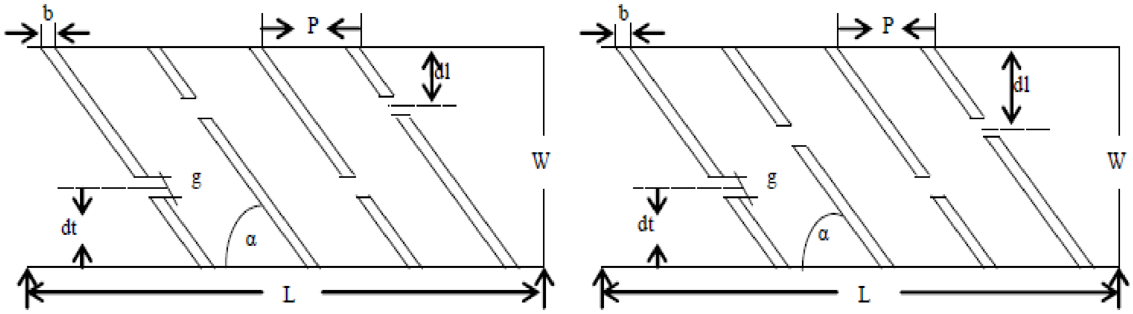


Fig.1. showing the geometric dimension of the working model



(a) dt/W & dl/W = 0.3 & 0.1 (b) dt/W & dl/W = 0.3 & 0.2



(c) dt/W & dl/W = 0.3 & 0.3 (d) dt/W & dl/W = 0.3 & 0.4

Fig. 2 Geometry of inclination rib with a gap in staggered arrangement

Complete duct geometry is divided into three sections, namely, entrance section, test section and exit section. A short entrance length is chosen because for a roughened duct, the thermally fully developed flow is established in a short length 2–3 times of hydraulic diameter. The exit section is used after the test section in order to reduce the end effect in the test section. The top wall consists of a 0.5 mm thick absorber plate made up of aluminum. Artificial roughness in the form of small diameter galvanized iron (G.I) wires is considered at the underside of the top of the duct on the absorber plate to have roughened surface, running perpendicular to the flow direction while other sides are considered as smooth surfaces. A uniform heat flux of 1000 w/m^2 is considered for computational analysis.

Fig no 2 Schematic diagram inclination rib with a gap in staggered arrangement

The 3-dimensional solution domain used for CFD analysis has been generated in ANSYS version 14.5 as shown in Fig.3.The solution domain is a horizontal duct with inclination rib with a gap in staggered arrangement on the absorber plate at the underside of the top of the duct while other sides are considered as smooth surfaces.

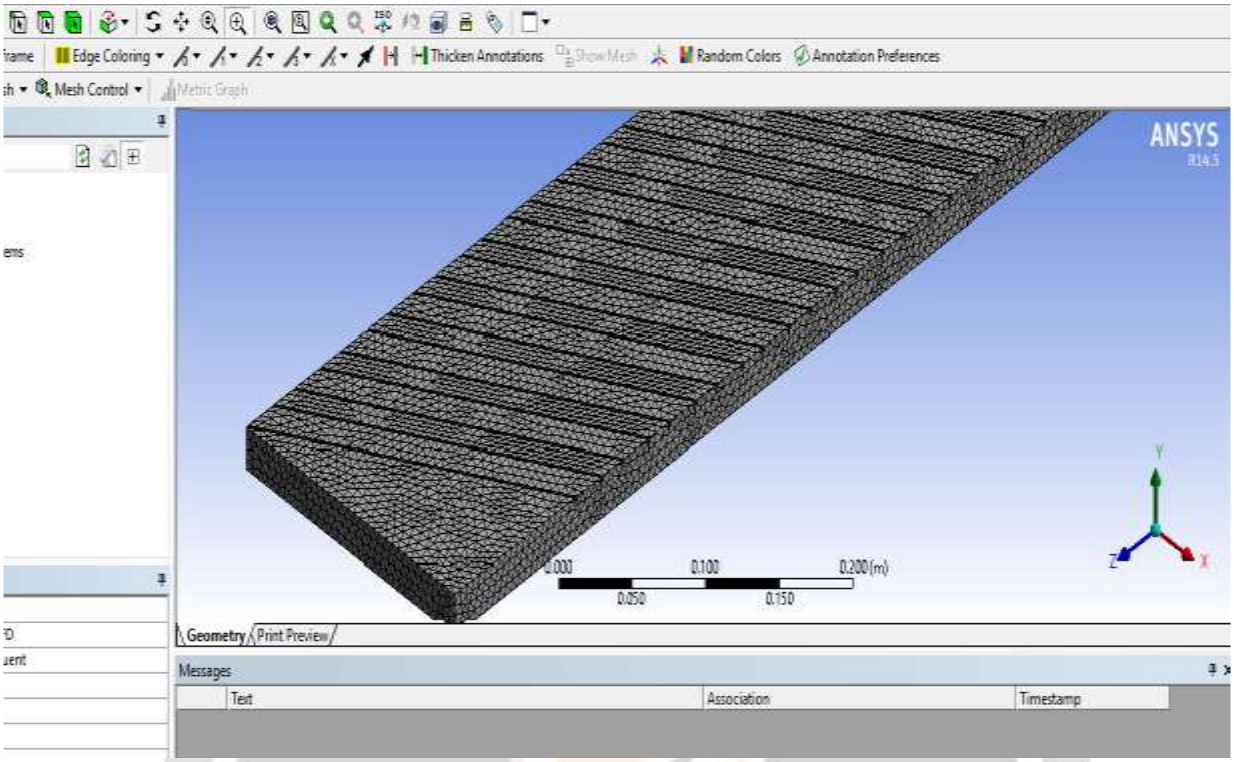


Figure 3. Meshing of duct with roughened absorber plate

In the present simulation governing equations of continuity, momentum and energy are solved by the finite volume method in the steady-state regime. The numerical method used in this study is a segregated solution algorithm with a finite volume-based technique. The governing equations are solved using the commercial CFD code, ANSYS Fluent 14.5. A second-order upwind scheme is chosen for energy and momentum equations. The SIMPLE algorithm (semi-implicit method for pressure linked equations) is chosen as scheme to couple pressure and velocity. The convergence criteria of $10^{-3}$for the residuals of the continuity equation, 10^{-6} for the residuals of the velocity components and 10^{-6} for the residuals of the energy are assumed. A uniform air velocity is introduced at the inlet while a pressure outlet condition is applied at the outlet. Adiabatic boundary condition has been implemented over the bottom duct wall while constant heat flux condition is applied to the upper duct wall of test section.

III. RESULTS AND DISCUSSION

A. Heat Transfer Characteristics and Friction Factor Characteristics

Fig.4 shows the effect of Reynolds number on average Nusselt number for different values of relative gap position (dt/W & dl/W) and fixed value of roughness pitch (*P*). The average Nusselt number is observed to increase with increase of Reynolds number due to the increase in turbulence intensity caused by increase in turbulence kinetic energy and turbulence dissipation rate.

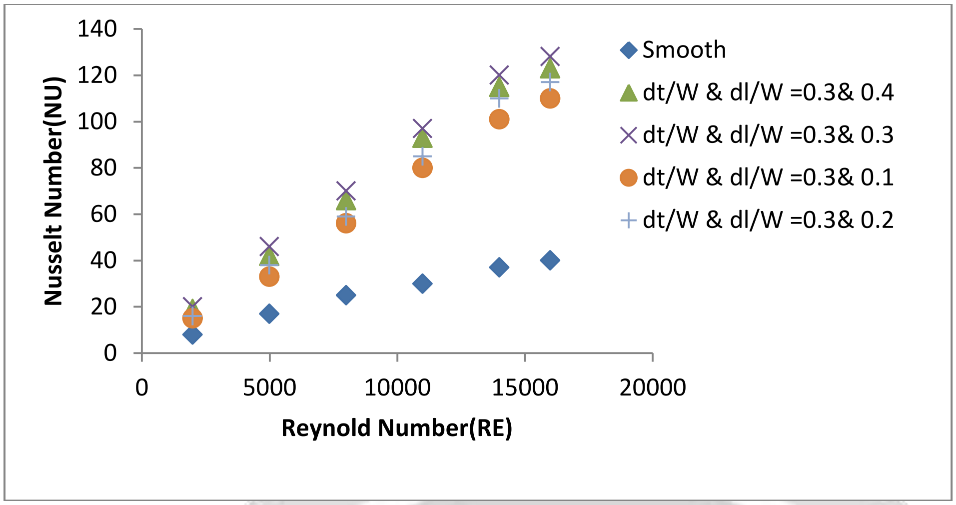
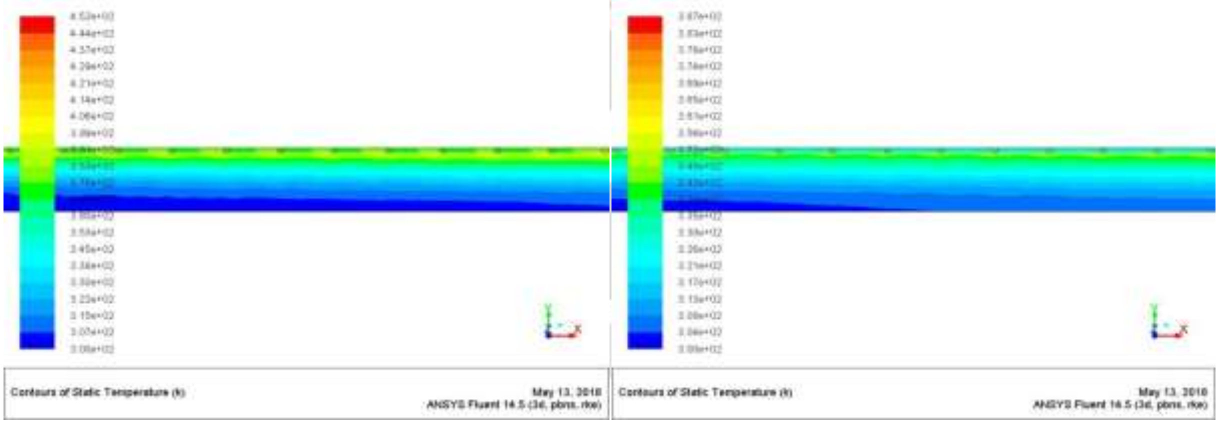
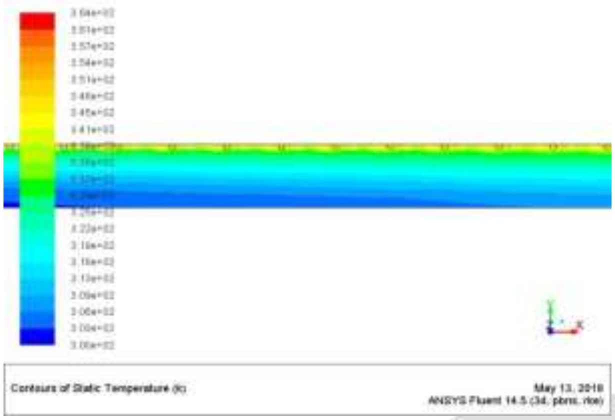


Fig. 4.Variation of Nusselt number with Reynolds number for different Values of combination of relative gap position (dt/W & dl/W)

Effect of the relative gap position (dt/W & dl/W) on heat transfer is also shown typically in Fig. 4.It can be seen that the enhancement in heat transfer of the roughened duct with respect to the smooth duct also increases with an increase in Reynolds number. It can also be seen that Nusselt number values increases with the increase in relative gap position (dt/W & dl/W) of up to 0.3&0.3 and than decrease for a fixed value of roughness pitch (*P*). The roughened duct having inclination rib with a gap in staggered arrangement with relative gap width (g/e) of 1 provides the highest Nusselt number at a Reynolds number of 16000. For rectangular rib the maximum enhancement of average Nusselt number is found to be 2.67 times that of smooth duct for relative gap width position (dt/W & dl/W) of 0.3&0.3 at a Reynolds number of 16000.The heat transfer phenomenon can be observed and described by the contour plot of turbulence intensity. The contour plot of turbulence intensity for inclination rib with a gap in staggered arrangement is shown in Fig.5 (a, b and c).The intensities of turbulence are reduced at the flow field near the rib and wall and a high turbulence intensity region is found between the adjacent ribs close to the main flow which yields the strong influence of turbulence intensity on heat transfer enhancement.



(a) **(b)**



(c)

Fig. 5 Contour plot of turbulent intensity for circular rib (a) Re=4000 (b) Re=8000 (c) Re=12000

Fig.6 shows the effect of Reynolds number on average friction factor for different values of relative gap position (dt/W & dl/W) and fixed value of roughness pitch. It is observed that the friction factor decreases with increase in Reynolds number because of the suppression of viscous sub-layer.

Fig 6 also shows that the friction factor decreases with the increasing values of the Reynolds number in all cases as expected because of the suppression of laminar sub-layer for fully developed turbulent flow in the duct. It can also be seen that friction factor values increase with the increase in relative gap width position (dt/W & dl/W) up to 0.3 &0.3 and than decrease for fixed value of roughness pitch, attributed to more interruptions in the flow path.

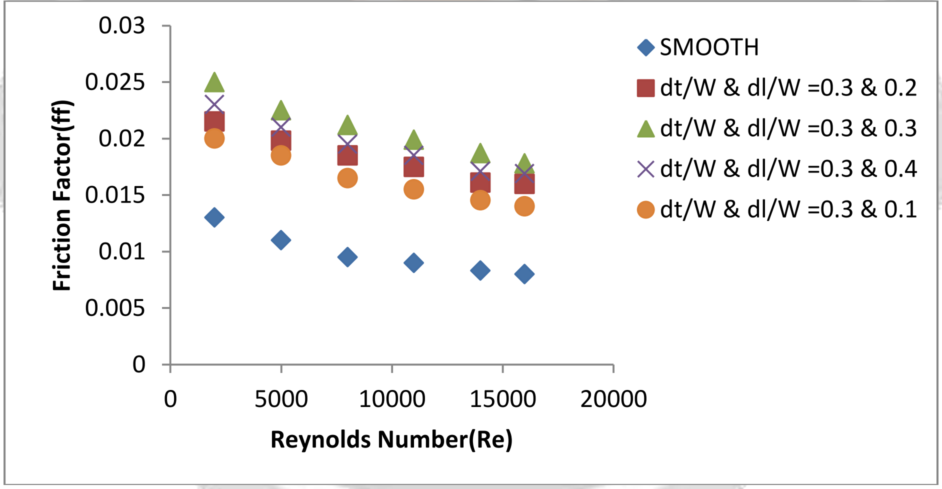


Fig. 6 Comparison between Friction factor and Reynolds number at different gap position (dt/W & dl/W)

B. Thermo-Hydraulic Performance

It has also been observed from Figures 4 and 6 that the maximum values of Nusselt number and friction factor correspond to relative gap position of 0.3 &0.3, thereby, meaning that an enhancement in heat transfer is accompanied by friction power penalty due to a corresponding increase in the friction factor. Therefore, it is essential to determine the effectiveness and usefulness of the roughness geometry in context of heat transfer enhancement and accompanied increased pumping losses. In order to achieve this objective, Webb and Eckert proposed a thermo-hydraulic performance parameter ‘η’, which evaluates the enhancement in heat transfer of a roughened duct compared to that of the smooth duct for the same pumping power requirement and is defined as,

$$\text{Thermal enhancement factor} = \frac{{}^{Nu}/_{Nu_s}}{\left({}^{f}/_{f_s}\right)^{\frac{1}{3}}}$$

The value of this parameter higher than unity ensures that it is advantageous to use the roughened duct in comparison to smooth duct. The thermo-hydraulic parameter is also used to compare the performance of number of roughness arrangements to decide the best among these. The variation of thermo-hydraulic parameter as a function of Reynolds number for different values of relative gap position and investigated in this work has been shown in Fig. 7. For all values of relative gap position, value of performance parameter is more than unity. Hence the performance of solar air heater roughened with inclination rib with a gap in staggered arrangement is better as compared to smooth duct.

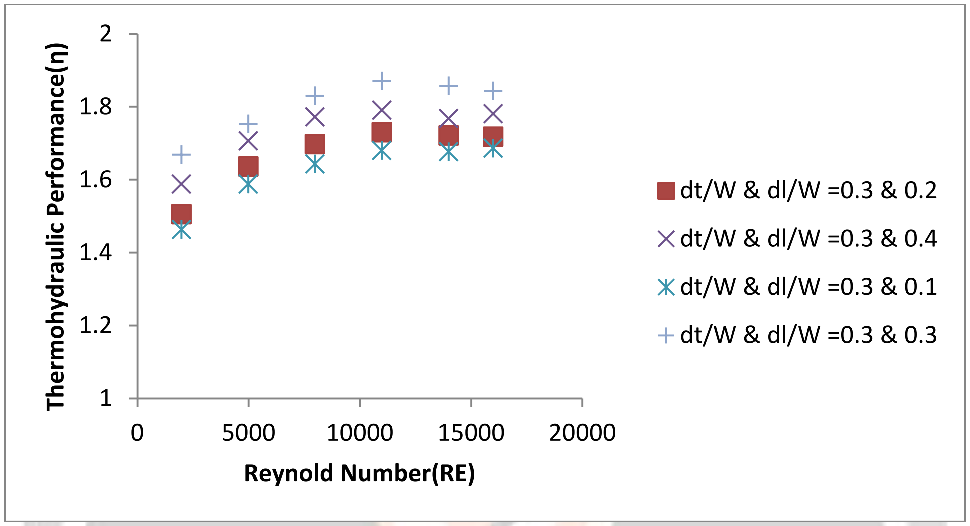


Fig.5 Thermo-hydraulic performance parameter as a function of Reynolds Number for different relative gap position (dt/W & dl/W)

It is also observed that the value of this parameter is maximum corresponding to relative gap position of 0.3 &0.3 and it decreases on both sides of this gap width for all values of Reynolds number investigated. This result indicates that it is advantageous to use inclination rib with a gap in staggered arrangement piece having gap position equaled to 0.3 &0.3 as compared to other values of relative gap widths. The highest value of thermo-hydraulic performance parameter obtained is 2.11 at Reynolds number of 11000.

Conclusion:

The Numerical investigations were conducted on solar air heater duct roughened with inclination rib with a gap in staggered. The following conclusions are drawn from the present study:

1. The roughened duct having inclination rib with a gap in staggered with relative gap position of 0.3 &0.3 provides the highest Nusselt number at a Reynolds number of 16000.
2. For rectangular rib the maximum enhancement of average Nusselt number is found to be 2.67 times that of smooth duct for relative gap position of 0.3 &0.3 at a Reynolds number of 11000.
3. The roughened duct having inclination rib with a gap in staggered with relative gap position of 0.3 &0.3 provides the highest friction factor at a Reynolds number of 3500.
4. For inclination rib with a gap in staggered the maximum enhancement of average friction factor is found to be 3.21 times that of smooth duct for relative gap position of 0.3 &0.3.
5. It is found that the thermal hydraulic performance of relative gap position of 0.3 &0.3 is maximum..

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